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Synchronization in a Class of Fractional-order Chaotic Systems via Feedback Controllers: a Comparative Study

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ABSTRACT

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Keywords:

Fractional-order chaotic system Proportional control Nonlinear fractional-order PI control Active control Master-slave synchronization Equivalent electronic circuit In this paper a synchronization methodology of two fractional-order chaotic oscillators under the framework of identical synchronization and master-slave configuration is introduced. The proposed methodology is based on a fractional-order feedback control design under the frame of control theory, the feedback controllers provide synchronization convergence. A comparative study between a proportional control, a nonlinear fractional-order proportional-integral control and an active control is presented. The above is showed via an analysis of the dynamic of the called synchronization error. Numerical experiments using the mathematical model of the fractional-order unified chaotic system and its equivalent electronic circuit corroborate the satisfactory results of the proposed schemes.

1 Introduction

A significant development of chaos occurred after the publication by Lorenz [1] of a work related with the existence of non-periodic solutions in a model formed by nonlinear differential equations. Lorenz's contribution provided the interest in studying deterministic systems that generate dynamic trajectories strongly influenced by sensitivity to initial conditions. However, it was until 1975 when the term chaos was introduced [2], since then chaotic systems have been studied intensively, and this is one important area of current research in physics, mathematics, and engineering. The analysis of nonlinear complex dynamic behaviors has led to important technological application. In particular the analysis of chaotic oscillators has had important advances in process engineering, cryptography of images, secure data transmission, life science, and information processing, between others [3]–[5].

There are several definitions about chaotic systems. However, in general terms, a chaotic system is a deterministic dynamic system that exhibits irregular behavior, similar to random behavior [6, 7]. A very important aspect in relation to chaos theory is the synchronization of chaotic systems. Since Pecora and Carrol [8] showed

that two seemingly random and unpredictable chaotic behaviors can converge in a single trajectory, new expectations arose around chaos theory, trying to solve its control, understanding and prediction.

The synchronization of chaotic systems consists of coupling two or more chaotic systems, after a transitory time, they exhibit identical chaotic oscillations. Synchronization can be solved from the point of view of control theory, designing a slave system which follows the variables of the master system. In the open literature has been presented a lot of important contributions for the design of control schemes for synchronization purposes in chaotic oscillators [9]–[11], observer based controllers [12, 13], adaptive algorithms [14, 15], optimal controllers [16, 17] and so on [18]–[20].

From the above, control theory has been looking for advanced techniques in order to reach a high performance in the operation of processes, in particular with dynamic systems with complex behavior, such as the nonlinear fractional-order systems [21]–[23]. The fractional calculus for the study of dynamic systems with chaotic behavior has emerged as an alternative framework, since it has been proved that it is possible that a class of systems exhibits chaos despite its order is fractional [24]–[27]. Generally, nonlinear systems display complex dynamic behavior as steady state multiplicity, in-

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stabilities, complex oscillations and so on under different initial conditions, external disturbances and time-varying parameters, leading to chaotic dynamic behaviors. However, besides of the scientific interest on the study and analysis of nonlinear system with exotic dynamic behaviors, the applications for engineering purposes have been growing importantly [28]–[31].

There are many engineering applications based on dynamical systems with fractional operators, for instance: fractional modelling of the human arm dynamics [32], modelling and identification of viscoelastic mechanical systems [33], modelling of electrical systems [34], analysis and control of economics and financial systems [35, 36], vibration and acoustics phenomena [37], modeling of friction in electric machines [38], problems in electrochemistry, biophysics and bioengineering [39]–[41], methods for signal and image processing [42, 43], applications in automatic control, mechatronics and robotics [44]–[46], among others [47]–[51]. However, there are a few practical applications in this field to prove the feasibility of the physical realization of the proposed techniques [52]–[54]. Some works deal with the master-slave synchronization of fractional-order systems via unidirectional linear coupling [55]–[58], where the proposed methods are applied in the synchronization of fractional-order Rössler, Chua, Chen, unified systems and so on.

The main contribution of this work is to achieve the synchronization of a class of fractional-order systems and its verification via the equivalent electronic circuit by means of a proportional control, a nonlinear fractional-order proportional-integral control and an active control. The synchronization implies that all trajectories of the slave system tend to follow all trajectories of the master system. In this sense, the main problem is to find a control input such that the synchronization is possible. The suitable conditions for the synchronization are obtained by solving the dynamical equation of the synchronization error. Furthermore, to verify the effectiveness of the suggested approach we have implemented an electronic circuit using Matlab-Simulink's Simscape library to obtain the synchronization regime between two fractional-order unified chaotic systems for the same order.

2 Fractional-order feedback controllers

The master system of fractional order α can be represented by,

$$D^{\alpha}x_i = f_i(x_1, x_2, \dots, x_n), \tag{1}$$

with $x_i(0) = x_{i0}$, i = 1, 2, ..., n, $x = [x_1, x_2, ..., x_n]^T \in \Omega \subset \mathbb{R}^n$ is the state vector, and $f : \Omega \to \mathbb{R}^n$ is a nonlinear continuous function.

In (1), the fractional derivative of x_i is defined as [?],

$$D^{\alpha}x_{i} = {}_{t_{0}}D^{\alpha}_{t}x_{i}(t) = \frac{d^{\alpha}x_{i}(t)}{dt^{\alpha}}$$
$$= \frac{1}{\Gamma(m-\alpha)}\int_{t_{0}}^{t}\frac{d^{m}x_{i}(\tau)}{d\tau^{m}}(t-\tau)^{m-\alpha-1} d\tau,$$
(2)

where: $\alpha \in \mathbb{R}^+$, $m - 1 \le \alpha < m$, $m \in \mathbb{N}$, $\frac{d^m x_i(\tau)}{d\tau^m}$ is the *m*-th time derivative of x_i and Γ is the gamma function.

2.1 Proportional control

Let us propose the controlled slave system of fractional order α as follows,

$$D^{\alpha}z_i = f_i(z_1, z_2, \dots, z_n) + u_i$$
 (3)

$$u_i = k_i(x_i - z_i) \tag{4}$$

with $z_i(0) = z_{i0}$, i = 1, 2, ..., n, $z = [z_1, z_2, ..., z_n]^T \in \Omega \subset \mathbb{R}^n$ is the state vector of the slave system, and k_i is the proportional gain.

Let us define the synchronization error as,

$$\varepsilon_i = x_i - z_i. \tag{5}$$

The synchronization performance is obtained by means of the analysis of the dynamics of the synchronization error.

First, we take the time derivative of order α of (5),

$$D^{\alpha}\varepsilon_{i} = D^{\alpha}x_{i} - D^{\alpha}z_{i} \tag{6}$$

Now, replacing the fractional dynamics of equations (1) and (3) into (6),

$$D^{\alpha}\varepsilon_{i} + k_{i}\varepsilon_{i} = f_{i}(x) - f_{i}(z)$$
(7)

Then, the solution of (7) is given by,

$$\varepsilon_{i}(t) = \varepsilon_{i0}E_{\alpha}(-k_{i}t^{\alpha}) + \int_{0}^{t} (t-\tau)^{\alpha-1}E_{\alpha,\alpha}(k_{i}(t-\tau)^{\alpha})\left[f_{i}(x) - f_{i}(z)\right]d\tau$$
(8)

where $\varepsilon_{i0} = x_{i0} - z_{i0}$.

In (8), the Mittag-Leffler function is defined as [?],

$$E_{\alpha}(q) = \sum_{j=0}^{\infty} \frac{q^j}{\Gamma(\alpha j+1)}, \quad q \in \mathbb{C}, \ \mathbb{R}e(\alpha) > 0$$
(9)

$$E_{\alpha,\alpha}(q) = \sum_{j=0}^{\infty} \frac{q^{i}}{\Gamma(\alpha j + \alpha)}, \quad q, \, \alpha \in \mathbb{C}, \, \mathbb{R}e(\alpha) > 0 \qquad (10)$$

To guarantee the convergence of the synchronization error in (8), Assumption 1 and 2 are introduced,

Assumption 1 $|f_i(x) - f_i(z)| \le L_i < \infty$

Assumption 2 The proportional gain is positive.

Applying Assumption 1 in (8) we have,

$$\begin{aligned} |\varepsilon_i(t)| &\leq |\varepsilon_{i0} E_\alpha(-k_i t^\alpha)| + \\ &+ L_i \int_0^t |(t-\tau)^{\alpha-1} E_{\alpha,\alpha}(-k_i (t-\tau)^\alpha)| \mathrm{d}\tau \end{aligned}$$

Finally, by Assumption 2,

$$\lim_{t \to \infty} |\varepsilon_i(t)| \le \frac{L_i}{k_i} \tag{11}$$

From the previous analysis, the following proposition is established.

Proposition 1 If Assumptions 1 and 2 are fulfilled, then the synchronization of the master system (1) and the controlled slave system (3)-(4) is achieved, where, the trajectories of ε_i belongs to a closed ball with radius proportional to L_i/k_i .

2.2 Nonlinear fractional-order PI control

Let us consider (1) as the master system. In this case, the slave system is described by,

$$D^{\alpha}z_i = f_i(z_1, z_2, \dots, z_n) + u_i, \quad i = 1, 2, \dots, n$$
 (12)

$$u_i = f_i(x) - f_i(z) + k_i \varepsilon_i + K_{I_i} e_i$$
(13)

$$D^{\alpha}e_i = \varepsilon_i \tag{14}$$

where, $\varepsilon_i = x_i - z_i$, k_i is the proportional gain and K_{I_i} is the integral gain.

Property 1 (see [59]) Let I^{α} be the fractional integral of order α . Then,

$$I^{\alpha}(D^{\alpha}e_i) = e_i \tag{15}$$

Applying Property 1 in both sides of (14),

$$e_i = I^{\alpha}(D^{\alpha}e_i) = I^{\alpha}\varepsilon_i \tag{16}$$

We analyze the dynamics of the synchronization error,

$$D^{\alpha}\varepsilon_{i} = f_{i}(x_{1}, x_{2}, \dots, x_{n}) - f_{i}(z_{1}, z_{2}, \dots, z_{n}) - u_{i}$$
(17)

$$u_i = f_i(x) - f_i(z) + k_i \varepsilon_i + K_{I_i} e_i$$
(18)

$$D^{\alpha}e_i = \varepsilon_i \tag{19}$$

Proposition 2 Let P be a matrix defined by,

$$P = \left[\begin{array}{cc} -k_i & -k_{I_i} \\ 1 & 0 \end{array} \right]$$

For $0 < \alpha < 1$, the interconnected system (17)-(19) is asymptotically stable if,

$$|arg(eig(P))| > \frac{\alpha \pi}{2} \tag{20}$$

where, eig(P) are the eigenvalues of P.

Proof. The closed-loop system could be expressed as,

$$\begin{bmatrix} D^{\alpha}\varepsilon_{i} \\ D^{\alpha}e_{i} \end{bmatrix} = \underbrace{\begin{bmatrix} -k_{i} & -k_{I_{i}} \\ 1 & 0 \end{bmatrix}}_{P} \begin{bmatrix} \varepsilon_{i} \\ e_{i} \end{bmatrix}$$
(21)

The eigenvalues of P are obtained in terms of proportional and integral gains,

$$eig(P) = \frac{-k_i \pm \sqrt{k_i^2 - 4K_{I_i}}}{2}$$

Hence, (21) is asymptotically stable if $|arg(eig(P))| > \frac{\alpha \pi}{2}$.

2.3 Active control

Let us represent the master system (1) as,

$$D^{\alpha}x = Ax + g(x), \tag{22}$$

In (22), $g : \Omega \to \mathbb{R}^n$ is a nonlinear continuous function and the matrix $A \in \mathbb{R}^{n \times n}$ is defined by,

$$A = \begin{bmatrix} a_{11} & a_{12} & \cdots & a_{1n} \\ a_{21} & a_{22} & \cdots & a_{2n} \\ \vdots & \vdots & & \vdots \\ a_{n1} & a_{n2} & \cdots & a_{nn} \end{bmatrix} = \begin{bmatrix} A_1 \\ A_2 \\ \vdots \\ A_n \end{bmatrix}$$
(23)

where, a_{ij} are constant coefficients and $A_i = \begin{bmatrix} a_{i1} & a_{i2} & \cdots & a_{in} \end{bmatrix}$ denotes the i-th row of matrix A, for i = 1, 2, ..., n.

Then, master system (22) can be rewritten as,

$$D^{\alpha}x_{i} = A_{i}x + g_{i}(x)$$

= $\sum_{j=1}^{n} a_{ij}x_{j} + g_{i}(x), \quad i = 1, 2, ..., n$ (24)

The corresponding slave system is proposed as,

$$D^{\alpha}z_{i} = \sum_{j=1}^{n} a_{ij}z_{j} + g_{i}(z) + u_{i}, \quad i = 1, 2, \dots, n$$
 (25)

Then, the dynamics of the synchronization error is obtained by (24) and (25),

$$D^{\alpha}\varepsilon_{i} = \sum_{j=1}^{n} a_{ij}\varepsilon_{j} + g_{i}(x) - g_{i}(z) - u_{i}, \quad i = 1, 2, \dots, n$$
(26)

Proposition 3 Equation (26) is asymptotically stable if the signal u_i is active,

$$u_i = \sum_{j=1, \ j \neq i}^n a_{ij} \varepsilon_j + g_i(x) - g_i(z) + k_i \varepsilon_i, \quad i = 1, 2, \dots, n$$
(27)

and the following condition is satisfied,

$$k_i > a_{ii} \tag{28}$$

Proof. Substituting 27 into (26),

$$D^{\alpha}\varepsilon_{i} = (-k_{i} + a_{ii})\varepsilon_{j}, \quad i = 1, 2, \dots, n$$
(29)

or, in matrix form

$$D^{\alpha}\varepsilon = \underbrace{\begin{bmatrix} -k_1 + a_{11} & 0 & \dots & 0 \\ 0 & -k_2 + a_{22} & & \vdots \\ \vdots & & \ddots & 0 \\ 0 & \dots & 0 & -k_n + a_{nn} \end{bmatrix}}_{\bar{A}} \varepsilon \quad (30)$$

Matrix \overline{A} is Hurwitz stable if $k_i > a_{ii}$, i = 1, 2, ..., n. Then (30) is asymptotically stable.

3 The fractional-order unified chaotic system

Consider the fractional-order master system [54],

$$D^{\alpha} x_{1} = (25\beta + 10)(x_{2} - x_{1})$$

$$D^{\alpha} x_{2} = 28x_{1} - x_{2} + 29\beta x_{2} - 35\beta x_{1} - 10x_{1}x_{3}$$

$$D^{\alpha} x_{3} = 10x_{1}x_{2} - \frac{\beta + 8}{3}x_{3}$$

(31)

With $\beta = 1$ and $\alpha = 0.9$ system (31) exhibits chaotic behaviour, in the sense of Definition 1.

Definition 1 ([6]) An attractor is said to be chaotic if it is bounded and all the trajectories starting form it are Lyapunov unstable. Then, a dynamic system is chaotic if it has at least one chaotic attractor.

System (31) is simulated through the Matlab-Simulink diagram shown in Figure 1, where blocks F1, F2 and F3 correspond to the approximation of the integral operator with order $\alpha = 0.9$.

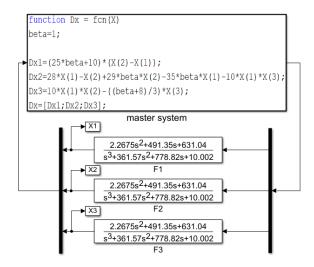


Figure 1: Simulation of system (31) using Matlab-Simulink

For simulation purposes, initial condition of block F1, was set to -0.001. Figure 2 shows the numerical simulation of system (31) via the phase portraits.

Now, in order to illustrate the behavior of system (31), we change the weight parameters (α , β). The simulation results are given in Figure 3 with parameters: (a) $\alpha = 0.9$, $\beta = 0$, (b) $\alpha = 0.9$, $\beta = -1$, (c) $\alpha = 0.8$, $\beta = 0.5$ and (d) $\alpha = 0.7$, $\beta = 1$. Clearly, system (31) is not chaotic with these set of parameters, where the integral operator with orders $\alpha = 0.8$ and $\alpha = 0.7$ is defined by [24],

$$\frac{1}{s^{0.8}} \approx \frac{5.235s^3 + 1453s^2 + 5306s + 254.9}{s^4 + 658.1s^3 + 5700s^2 + 658.2s + 1}$$
(32)

and

$$\frac{1}{s^{0.7}} \approx \frac{5.406s^4 + 177.6s^3 + 209.6s^2 + 9.197s + 0.01450}{s^5 + 88.12s^4 + 279.2s^3 + 33.30s^2 + 1.927s + 0.0002276}$$
(33)

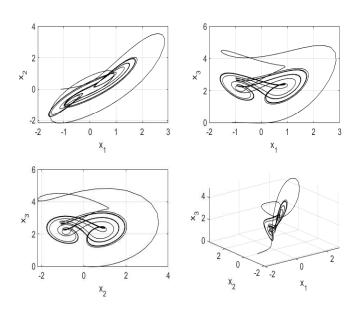


Figure 2: Simulation results of system (31), $\beta = 1$ and $\alpha = 0.9$.

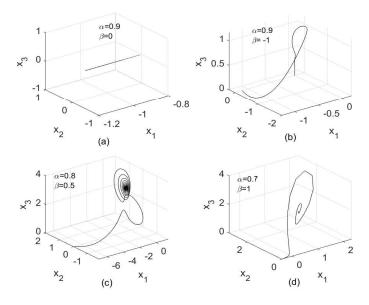


Figure 3: Phase portraits of system (31) with different values of (α, β) ...

4 Synchronization results and discussion

The fractional-order slave system that synchronizes with system (31) is represented as,

$$D^{\alpha}z_{1} = (25\beta + 10)(z_{2} - z_{1}) + u_{1}$$

$$D^{\alpha}z_{2} = 28z_{1} - z_{2} + 29\beta z_{2} - 35\beta z_{1} - 10z_{1}z_{3} + u_{2}$$

$$D^{\alpha}z_{3} = 10z_{1}z_{2} - \frac{\beta + 8}{3}z_{3} + u_{3}$$
(34)

where $\beta = 1$, $\alpha = 0.9$ and u_1 , u_2 and u_3 are the control signals.

It is necessary to calculate the control gains values. First, for the proportional control, we obtain the constants L_i over the bounded set $\Omega = \{x \in \mathbb{R}^n \mid |x_i| \le M_i\},\$

$$L_{i} = \max_{1 \le i \le n} \|f_{i}'(x)\|$$
(35)

where $f'_i(x)$ is the Jacobian matrix.

Then, considering that $M_1 \approx 2$, $M_2 \approx 3$ and $M_3 \approx 4$, we have that $L_1 = 35$, $L_2 = 47$, and $L_3 = 30$.

According to Proposition 1, the maximum synchronization errors are defined as

$$\varepsilon_{i_{\max}} = \frac{L_i}{k_i} = 0.05 \tag{36}$$

In Equation (36) we consider the synchronization errors are bounded by 0.05, they are acceptable for complete practical synchronization. Equation (36) yields to $k_1 = 700$, $k_2 = 940$, and $k_3 = 600$.

For the nonlinear PI controller, the gain values are obtained in order to guarantee a settling time of 0.02s and an overshoot of 1% in the three coordinates, then ki = 400 and $K_{I_i} = 58613$, for i = 1, 2, 3. And for the active controller we have the following conditions,

$$k_1 > -25\beta + 10$$
 (37)

$$k_2 > 29\beta - 1 \tag{38}$$

$$k_3 > -\frac{\beta+8}{3} \tag{39}$$

In this case, we choose $k_1 = 200$, $k_2 = 100$ and $k_3 = 100$.

Figure 4 shows the phase portraits of the master and slave systems when the control signals are off, clearly all systems are unsynchronized due to the initial conditions are different. However, when the feedback controllers are activated the synchronization is achieved since the trajectories of the controlled slave system tend to follow the trajectories of the master system.

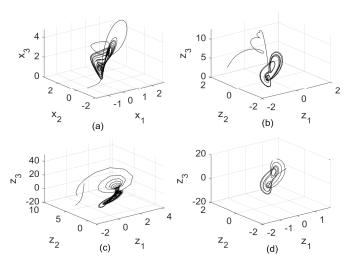


Figure 4: Unsynchronized systems.

In Figure 5 the synchronization performance is verified via the synchronization errors. We observe that the synchronization errors converge to zero when the feedback control is activated. As we can

note, the corresponding slave trajectory reach almost immediately the master trajectory for the proportional control, also, when the nonlinear PI control acts, the corresponding trajectory has a higher oscillatory overshoot and a settling time of 0.02s, and for the active control, the synchronization errors converge exponentially to zero at 0.02 s.

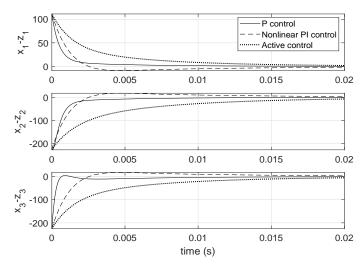


Figure 5: Synchronization errors.

The above-mentioned behaviors for the state variables under feedback controllers can be explained for the performance of the three controllers under comparison. Figure 6 is related to the control effort performance, it can be observed that the control effort for the proportional controller is very high due to the magnitude presented at the startup and transient condition. On the other hand, PI and active controllers show a smooth behavior, leading the trajectory to the controlled slave system to the required master trajectory in a larger settling time.

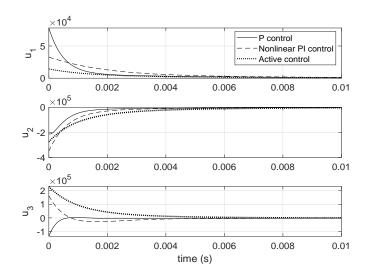


Figure 6: Control signals.

5 Equivalent electronic circuit

System (31) is translated to the electric circuit shown in Figure 7.

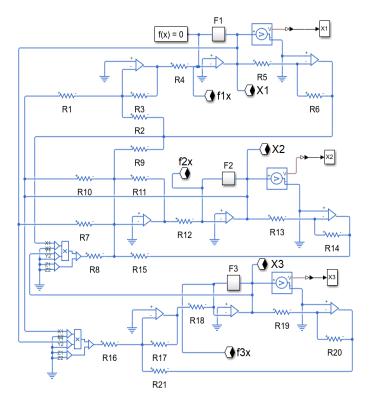


Figure 7: Electrical model of master system (31) using Simulink's Simscape library.

Component values are taken as: $R_4 = R_{13} = R_{18} = 100 k\Omega$, $R_1 = R_5 = R_7 = R_8 = R_{10} = R_{14} = R_{16} = R_{20} = 10 k\Omega$, $R_2 = R_3 = R_6 = R_{21} = 33 k\Omega$, $R_9 = R_{11} = R_{15} = 27 k\Omega$ and $R_{12} = R_{17} = R_{19} = 100 k\Omega$.

Fractional integrators blocks F1, F2 and F3 are represented as $\frac{1}{s^{0.9}}$. Figure 8 shows the approximation of $\frac{1}{s^{0.9}}$ as an electric circuit using the Simscape libraries.

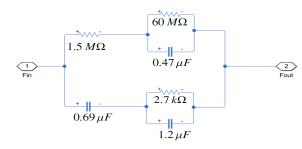


Figure 8: Integrator blocks F1, F2,..., F12.

6 Verification of the master-slave synchronization

The synchronization is verified via the equivalent electronic circuits of master and slave systems. The controlled slave electronic circuit is given in Figure 9, where u_1 , u_2 and u_3 are the control inputs

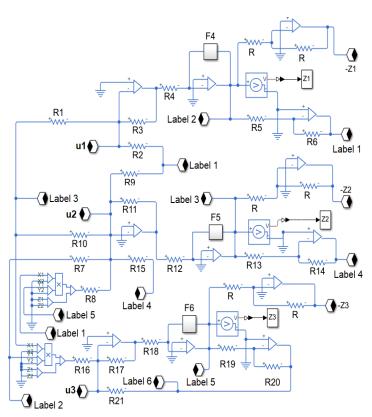


Figure 9: Electrical circuit schematic for the slave system (34).

Master circuit of Figure 7 and slave circuit of Figure 9 are coupled since the control inputs require information signals from both circuits.

The equivalent circuit for the proportional control (4) is shown in Figure 10. Resistors R_{P1} , R_{P2} and R_{P3} are related with the control gains of Section 4 as follows,

$$R_{P1} = 10\frac{R_3}{k_1} = 471 \ \Omega \tag{40}$$

$$R_{P2} = 10 \frac{R_{11}}{k_2} = 287 \,\Omega \tag{41}$$

$$R_{P3} = 10 \frac{R_{17}}{k_3} = 1.67 \text{ k}\Omega \tag{42}$$

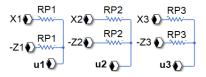


Figure 10: Proportional control.

The nonlinear fractional-order PI control (13)-(14) is proposed by means of the circuit of Figure 11.

where,
$$F_i(x) = \sum_{j=1, j \neq i}^n a_{ij} x_j + g_i(x)$$
 and $F_i(z) = \sum_{j=1, j \neq i}^n a_{ij} z_j + g_i(z)$.

R3

R2

R9

R11

R18

RF3

R17

R1

~~ R7

R16

F1x

R12

Label 3

Label2

Label5

R1

R7

R16

R8

R3

R2

R9

R11

R12

R17

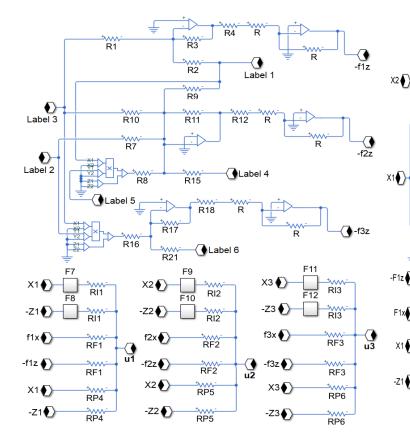


Figure 11: Nonlinear fractional-order PI control.

The parameter values are obtained as,

$$R_{P4} = 10\frac{R_3}{k_1} = 825 \ \Omega \tag{43}$$

$$R_{P5} = 10 \frac{R_{11}}{k_2} = 675 \,\Omega \tag{44}$$

$$R_{P6} = 10 \frac{R_{17}}{k_3} = 250 \ \Omega \tag{45}$$

$$R_{I1} = 10 \frac{R_3}{K_{I_1}} = 5.63 \ \Omega \tag{46}$$

$$R_{I2} = 10 \frac{R_{11}}{K_{I_2}} = 4.6 \,\Omega \tag{47}$$

$$R_{I3} = 10 \frac{R_{17}}{K_{I_3}} = 17 \,\Omega \tag{48}$$

$$R_{F1} = 10 R_3 = 330 \text{ k}\Omega \tag{49}$$

$$R_{F2} = 10 R_{11} = 270 \text{ k}\Omega \tag{50}$$

$$R_{F3} = 10 R_{17} = 1 M\Omega$$
 (51)

Finally, the equivalent circuit for the active control (27) is given by Figure 12. The active control (27) has been rewritten as,

$$u_i = F_i(x) - F_i(z) + k_i \varepsilon_i, \quad i = 1, 2, \dots, n$$
 (52)

Figure 12: Active control.

The corresponding parameter values are: $R_{F1} = 330 \text{ k}\Omega$, $R_{F2} = 270 \text{ k}\Omega$, $R_{F3} = 10 R_{17} = 1 \text{ M}\Omega$ and,

מ

$$R_{A1} = 10\frac{R_3}{k_1} = 1.65 \text{ k}\Omega \tag{53}$$

$$R_{A2} = 10 \frac{R_{11}}{k_2} = 2.7 \text{ k}\Omega \tag{54}$$

$$R_{A3} = 10 \frac{R_{17}}{k_3} = 10 \text{ k}\Omega \tag{55}$$

Figure 13 shows the phase portraits of the master-slave synchronization obtained by means of the equivalent electronic circuits given by Figures 7 and 9 along with the control inputs of Figures 10, 11 and 12. For all simulations, initial voltage on capacitor of 0.69 μF takes several arbitrary values: 1 V (block F1), -2 V (block F4), 1 V (block F5), 1 V (block F6), while the rest of capacitors remain at 0 V. Notably, the whole phase portrait of the controlled slave system is synchronized with the corresponding phase portrait of the master system using the proposed controllers, for arbitrary initial conditions. However, an important characteristic is that the nonlinear fractional-order PI control and the active control lead to complex circuit structures.

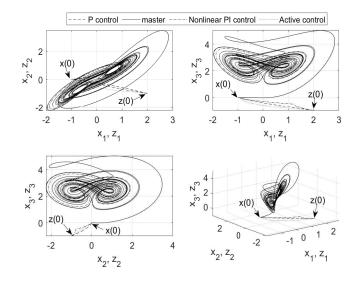


Figure 13: Master-slave synchronization.

7 Conclusions

This work studied the master-slave synchronization in a class of chaotic systems with fractional-order via feedback control. First, the feedback controllers were designed. In this sense, a proportional control was proposed, it guarantees that the synchronization error is bounded, as well as, a nonlinear fractional-order PI control and an active control were introduced, where the stability of the closed-loop system depends on the control gains, here for both controllers the synchronization error is asymptotically stable. Next, as application example, the fractional-order unified chaotic system was considered as master system. In fact, a set of numerical simulations based on the mathematical models of master and slave system showed that the synchronization is fulfilled by means of the proposed feedback controllers. It is important to mention that the proportional control exhibited the higher control effort, which could be a restriction in another class of systems, for instance, in those involving actuators. On other hand, in the transient condition, the active control is slower than the other ones. Finally, the synchronization was verified with success using the equivalent electronic circuits. As can be noticed, the proportional control has a simple circuit structure.

Conflict of interest The author declares no conflict of interest.

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