2x1 Microstrip Patch Array Antenna with Harmonic Suppression Capability For Rectenna

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ABSTRACT

This paper is an extension of work originally presented in 2016 IEEE Asia-Pacific Conference on Applied Electromagnetics (APACE). A 2×1 microstrip patch array antenna integrated with photonic bandgap (PBG) and stubs is designed and analyzed. The performance of the PBG and stubs structure are explained and analyzed in terms of the elimination of the resonance at the harmonic frequencies of the antenna. The proposed antenna is designed on FR-4 substrate with thickness of 1.6 mm and operated at 2.45 GHz frequency suitable for rectenna design application. From the simulated result, the first harmonic frequency (5.4 GHz), the second harmonic frequency (6.6 GHz) and the third harmonic frequency (7.8 GHz) are successfully suppressed. For instance, the radiation to the forward of the stubs-PBG antenna is suppressed at more than 15 dB at the second and third harmonic frequencies.

1. Introduction

The term rectenna is commonly denoted as rectifying antenna at microwave power transmission system. It is a combination of the antenna and high efficient rectifier circuit. The ability of the wireless power transmission system is very important and it depends on the ability of each process; the conversion of signal DC-to-RF at the transmitter, at the transmission and at the conversion of signal RF-to-DC at the receiver. Hence, the receiving antenna is one of the main elements in the rectenna system development.

One of the most popular types of receiving antenna that is used for rectenna application is the microstrip patch antenna [1 - 4]. Some of the advantages of employing this type of antenna is low profile, low cost, light-weight and suitable if integrated with RF devices. However, it also exhibits disadvantages such as the excitation of surface waves that exist in the substrate layer. Surface waves are exceptionable because when a patch antenna radiates, a part of the total available radiated power becomes trapped along the surface of the substrate. It will diminish the total available power for radiation to space wave, and the harmonic frequency is produced. In addition, for arrays antenna, surface waves have a significant impact on the mutual coupling between array elements [5]. Moreover, in rectifying circuit, diode that used to convert the RF signal to DC power supply also generates the unwanted radiation of harmonic frequencies. Thus, the rectenna cannot operate well and will disturb the overall performance of the system.

Several design methods have been proposed in the past in order to overcome these unwanted generated harmonic problems. One of the most popular methods is called the photonic band gap (PBG) or electromagnetic band gap (EBG) [6 - 8] and defected ground structure (DGS) [9 - 11]. Several other techniques for instance antenna with slit and stub structure [12], circular sector patch antenna [13], slot antenna and notch antenna [14], Low Pass Filter (LPF) [15 - 17] also have been discussed earlier as a one of the method to suppress the harmonic frequencies.

According to that, a harmonic suppression microstrip array patch antenna is proposed in order to improve the system performance. In this paper, the 2×1 microstrip patch array antenna integrated with stubs and two-dimensional (2-D) PBG pattern in the ground plane beneath the square patch, is proved experimentally and the capability of the stubs and PBG structure for the suppression of the harmonics are discussed [18].

2. Antenna design procedure

2.1. Numerical method

The structure of the microstrip patch array antenna with PBG substrate (PBG antenna) is presented in Figure 2. A 2×1 array antenna is fabricated on the FR-4 substrate with dimensions of 143 x 52 x 1.6 mm³ and the relative permittivity of εr = 4.4. The source signal is fed directly to the antenna by the 50Ω microstrip line with
width length (Wd2) = 4.13 mm. The rectangular inset feed antenna dimensions are calculated prior to designing the array antenna by using [19]:

\[ W = \frac{c}{2f_0 \sqrt{\varepsilon_{eff}}} \]  \hspace{1cm} (1)

\[ \varepsilon_{eff} = \frac{\varepsilon_r + 1}{2} + \frac{\varepsilon_r - 1}{2} \left( \frac{c}{f_0} \right)^2 \]  \hspace{1cm} (2)

\[ L_{eff} = \frac{c}{2f_0 \sqrt{\varepsilon_{eff}}} \]  \hspace{1cm} (3)

\[ \Delta L = 0.412h \frac{(\varepsilon_{eff}+0.3)(\varepsilon_{eff}+0.264)}{(\varepsilon_{eff}+0.258)(\varepsilon_{eff}+0.8)} \]  \hspace{1cm} (4)

\[ L = L_{eff} - 2\Delta L \]  \hspace{1cm} (5)

Where:

- \( W \) = Width of the patch
- \( L \) = Length of the patch
- \( \varepsilon_r \) = Dielectric constant of substrate
- \( \varepsilon_{eff} \) = Effective dielectric constant of substrate
- \( c \) = Speed of light
- \( f_0 \) = Frequency reference
- \( h \) = Height of dielectric substrate

There are advantages of PBG structure which are increasing the antenna’s performance in terms of the gain and radiation pattern and also react as a filter to suppress the harmonic frequency. The PBG structure is designed based on the formula [20]:

\[ \lambda = \frac{c}{f_0 \sqrt{\varepsilon_r}} \]  \hspace{1cm} (6)

\[ r = \lambda/8 \]  \hspace{1cm} (7)

\[ a = \lambda/2 \]  \hspace{1cm} (8)

After calculation, the 9 x 5 squares with the dimensions 7 x 7 mm² are etched in the ground plane at the period \( g_a \) of 15 mm as shown in Figure 1.

![PBG structure at ground plane](image)

2.2. Design simulation

By using CST microwave software, the rectangular inset feed antenna is designed and simulated to get the operating frequency at 2.45 GHz. Some enhancement are made to obtain the best performance of the antenna. After completing the single element geometry, a 2x1 array antenna is designed. The parameters of the feed line network can be chosen by setting the feed line impedance to 50 \( \Omega \) \( (Z_1 = 50 \Omega) \), which splits into two 100 \( \Omega \) \( (Z_2 = 100 \Omega) \) [21]. Similarly, some optimization is done in order to get the greatest achievement of the array antenna.

After done with the conventional microstrip patch array antenna design, the 9 x 5 PBG square are etched at the ground plane. However, some size optimization of PBG square size is done in order to match with the 2x1 array patch antenna design.

![2x1 microstrip patch array antenna with stubs and PBG structure](image)

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![Table 1: Dimension of antenna (unit: mm)](image)

3. Result and discussion

This proposed antenna is divided into three parts which are normal array patch antenna, PBG array antenna and array patch antenna with PBG and stub structure. Each part is discussed and analyzed according to their characteristics.

3.1. Normal array patch antenna

The normal patch antenna without PBG structure shows in Figure 3 is simulated and measured for the comparison of the basic
characteristics. The resonant frequency of the fundamental is adjusted to be 2.45 GHz for the antenna. The simulated and measured S-parameter (return loss) result of the array antenna without stubs and PBG structures are shown in Figure 4. As can see, the return loss is at -13 dB and has a few harmonic frequencies which are not good for an antenna.

3.2. PBG structure

As can see in Figure 4, there are a lot of harmonic frequencies produces above 4 GHz. Hence, PBG structure is beneath at the ground in order to suppress the harmonic frequencies. At the same time, the gain of the antenna also can be improved. Figure 5 shows the PBG structure at ground plane. This arrangement of the PBG lattice produces the band pass characteristics of the transmission parameter at more than -20 dB from 4.6 GHz to 8 GHz shown in Figure 6 (a) when the uniform microstrip line is fabricated on this substrate instead of the patch antenna. The effect of the PBG can be seen by observing the S-parameter (return loss) in Figure 6 (b). It shows that the harmonic frequencies above 4.6 GHz is successfully suppressed when the S-parameter of PBG structure is compare with return loss of 2x1 rectangular inset feed array antenna with and without PBG structure. While Figure 7 shows the comparison of return loss of 2x1 rectangular inset feed array antenna with PBG structure only between simulation and measurement.
3.3. Array patch antenna with PBG and stub structure

The final design is combination of normal array patch antenna with PBG and stubs structure as shown is Figure 8. The S-parameter (return loss) of the array antenna with PBG and stubs structure, and the array antenna without PBG and stubs structure are shown in Figure 9.

![Figure 8: Prototype of 2x1 rectangular inset feed array antenna with PBG structure and stub](image)

**Figure 8: Prototype of 2x1 rectangular inset feed array antenna with PBG structure and stub**

![Figure 9: Measured S-Parameter (return loss) of the proposed array antenna. Graph of the comparison for antenna with and without stubs and PBG](image)

**Figure 9: Measured S-Parameter (return loss) of the proposed array antenna. Graph of the comparison for antenna with and without stubs and PBG**

![Figure 10: Comparison of return loss between simulation and measurement for 2x1 array patch antenna with PBG and stub structure](image)

**Figure 10: Comparison of return loss between simulation and measurement for 2x1 array patch antenna with PBG and stub structure**

3.4. Gain

As mentioned before, besides suppressing the harmonic frequency, PBG structure also can increase the performance of the antenna in terms of gain. As can be seen in Figure 11 (a) and (b), there are comparison antenna’s gain between simulation and measurement for normal array patch antenna and PBG array patch antenna.

![Figure 11: Comparison of antenna’s gain between simulation and measurement (a) normal array patch antenna (b) PBG array patch antenna](image)

**Figure 11: Comparison of antenna’s gain between simulation and measurement (a) normal array patch antenna (b) PBG array patch antenna**

In Table 2, due to the effective suppression of the harmonic and the surface wave, and changes in the current distribution, the antenna array with stub and PBG has higher gain compared to the normal array antenna. The gain increase about 82.41% which is from 3.156 dB to 5.757 dB. While for normal array antenna and array antenna with PBG structure, the result shows a minimal gain increase by 36.66%. Thus, it shows that with the addition of stub structure at the feed line, the gain’s performance will improve more. Moreover, the mixed current distribution is useful for diminishing the mutual coupling between the patches and decreasing the maximum side-lobe level.
Table 2: Measured antenna gain base on structure added

<table>
<thead>
<tr>
<th>Antenna structure</th>
<th>Gain (dB)</th>
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<tbody>
<tr>
<td>Array antenna without PBG and stub</td>
<td>3.156</td>
</tr>
<tr>
<td>Array antenna with PBG</td>
<td>4.313</td>
</tr>
<tr>
<td>Array antenna with PBG and stub</td>
<td>5.757</td>
</tr>
</tbody>
</table>

4. Conclusion

2x1 microstrip patch array antenna has been presented in this effort. The proposed structure is integrated with two-dimensional PBG pattern in the ground plane under the square patch and stubs. The effectiveness of the PBG and stubs structure for harmonic suppression are analyzed. The simulation and measurement works verified that the combination of the array antenna with PBG and stubs is efficient in eliminating unwanted frequencies. Moreover, the performances of the antenna in term of gain also increase.

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References